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Table of contents

Marat Abdulganiev, Miroslava Ray: The energy of sheet bending on a crank-type press	3
denotes of the cooding of a sugar beet on the coefficient variation of intervals	8
C Poursime Dmitry Serbienko: Calculation of magnetic systems of speed	
I teath integrity concore	.13
Deletekova Alaksandr Kuschenko, Denis Kapustin: Experimental rescarch	
Classification appropriate and a solid fuel burning	.19
Description and principles	
of their modeling	23
architectures of the coal industry enterprises	51
The New Art Aria With the man Deculte of researches by the numeral methods	
of vertical influences on the way of carriages of industrial transport at the fainbad des 3D 3	50
Helen Demyanenko, Nina Mikhaylova: The study of physical and mechanical properties of labrics	
The development of the model of regional system	
c	44
Andrew Folklery Olena Norbenko: Passive safety features of parts produced by rapid prototyping technologies	49
Vil. torive Catchenko Vuriv Reletsky: Mathematical model of choice of the switcher's	
the system of two units on the system of two units on the basis of fuel fate diffinitioning	54
oritorion	54
Valedayete Nilita Reagin: Diesel-locomotive switcher's modernisation	
1 1 1 1 temporagion of nower	64
Ol - Coochyon Enrichability curves analysis of several coals mixture	04
4 - mining inductor	
Down Shovehenko: Operational aspects of screw feeder	
of transport gasifier with pellet burner	
Valleyman Dasic principles of the management of region as	
the ecological-economic system	85
Yuri Kossenko-Belinsky: Use of the numerical experiment at the design stage of piston pulp pumps	
Maksim Kovtanets, Nicholas Gorbunov, Olga Prosvirova, Sergei Sosnovenko, Vitali Astakhov:	
Increase of coupling characteristics and profitability of the locollotive modernization	90
of system of supply of sand	96
Yuriy Kozub: Deformation of rubber-metal vibration and seising isolators	
Alexander Krajniuk, Yuri Starcheous, Alexander Danileychenko, Maksim Bryantsev: Method of a choice of parameters of the air cooling machine of a cascade pressure exchange	101
Method of a choice of parameters of the air cooling machine of a cascade pressure status	
Catherine Kravchenko, Nikolai Gorbunov, Sergey Sosnovenko, Olga Prosvirova, Nikita Bragin: Influence of locomotive operating characteristics on wheels in contact with the rails	108
Influence of locomotive operating characteristics of wheels in contact with the	113
Vasiliy Kudlenko, Sergey Vorobjov: Cosmic rays muon detectionon the earth surface	
Oleg Lehtsier, Vitaly Ulshin, Oleg Kilymnik, Alexey Pismenskiy: Determination the dynamic parameters of the controlled technological processes of coal preparation by using the semi graphical method	117
of the controlled technological processes of coal preparation by using the serin graphical Nadezhda Makhortova, Yuri Vivdenko: Rail vehicle wheels common faults characterisic	123
Nadezhda Makhortova, Yuri Vivdenko: Kall venicle wheels common fauts characteriste mounter	127
Valeriy Maletkin, Oleg Druz, Lydmila Maletkina: Dangerous radiation when using your computer	
Igor Malkov, Gennadiy Sirovoy, Sergey Kashkarov, Igor Nepran: The analysis of adhesion effect on properties of the modified polymeric nano composites	

Dmitriy Marchenko: Investigation of the kinetics of the development of the distribution	134
Vitaliy Maximov, Svitlana Firsova, Irina Litvinova: Strategic controlling of innovation activities of enterprises in the changing technological structure of economy	
Gennadiy Mogilnuy, Vladimir Donchenko: Research of trajectory design error of coil piling	
of geodesic winding	145
Mohammad Alatoom: To the methodology of experimental research of the continuous-running fodder mixed Olga Mokshina, Oleksandr Riabchykov, Svetlana Chelysheva: The algorithms for improvement	
regulatory provision of light industry	
processes optimization.	162
Alexander Mukhovatiy: Synthesis of toothed gearing with reduced energy capacity	167
Evelina Musayeva, Inna Belaya: The prediction of myocardial infarction consequences as a result of vectorcardiography research using «Decision trees» data mining algorithm	171
technologies of the crankshaft engine rehabilitation	
Olena Nozhenko, Mykola Gorbunov, Valentyn Mogyla, Alexsander Pilatau, Vycheslav Chernikov, Andrey Anofriev: Ways to increase the energy efficiency of locomotives	
Volodymir Nozhenko, Nikolai Gorbunov, Sergey Mokrovsov, Vycheslay Chernikov, Maxim Koytonov	102
Rostislav Demin: Experimental measurement complex running gear for research and of interaction conditions rolling stock	100
Alexander Petrov, Sergey Velchenko: The mechanism of the analysis of entering Internet traffic for the presence of threats	
Vladimir Pilipenko: Mathematical model-building of reological and thermodynamical processes	
in modified concrete mix at vibro impact compact method of comression	204
Oleg Pogorelov: Outline of a theory of semantic information and misinformation	210
Natalia Pogrebnova: Estimation of frictional properties of the disc brake working elements in order to increase efficiency of brake systems of the rolling stock	218
Olga Porkuian, Igor Kurganov: Research of the automatic control system of belt conveyor on the technical basis of the industrial controller schneider electric	223
Vladimir Punagin: Physicochemical characteristics of bond and friction between the modified concrete and sliding formwork for the construction of high-rise buildings	
Valentin Rach, Alina Borzenko-Miroshnichenko: Features of project analysis of the project portfolio of regional educational space	
Sultan Ramazanov: Innovative management models of viable and stable development of technogenic region in crisis	
Sultan Ramazanov, Leonid Istomin, Alexey Dyubanov: Dynamic model of the competition	
in regional market of e-commerce enterprises	
waste products Ksieniia Sieriebriak: Informative and communicative technologies as a factor of increase industrial	
efficiency production: regional aspect	259
Yaroslav Sklifus, Valentin Mohyla: The results of the experimental research of the heat transfer coefficient during steam condensation in the tubes of the diesel radiator sections.	
Vladimir Sokolov, Nataliya Azarenko, Yana Sokolova: Simulation of the power unit of the automatic electrohydraulic drive with volume regulation	
Iosif Stentsel, Olga Porkuyan, Elena Prokaza: Researches of the system of neutralization process control	
in the production of ammonium nitrate on the basis of rheological transitions principles	274
Dmitry Syomin, Andrii Rogovyi: Mathematical simulation of gas bubble moving in central region of the short vortex chamber	279
Vitalij Ulshin, Victoria Smoliy, Yaroslav Fomyn: Mathematical design and operations of electronic vehicles management and introduction of results of researches in an educational process	285
Olexsander Verkhovodov, Olexsander Karpuyk: Development of control system of hydraulic press based on zelio logic controller	
Yuriy Vivdenko, Julia Krasnobryzheva: Control system of pneumatic air-spring suspension on transport	294

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Deformation of rubber-metal vibration and seismic isolators

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Summary. The different going is considered near the decision of task about the tensely-deformed state of rubbermetal vibration isolators are considered. The method of the solution of a task about deformation of constructions from nearly incompressible material on application moment scheme of finite elements is offered. For the decision of task of nonlinear viscoelasticity deformation of construction the newton-Kantorovich method is used.

Keywords: finite element method, vibration isolator, nearly incompressibility.

INTRODUCTION

The considerable part of the population of the globe lives in the seismoactive territory. Therefore protection of buildings, constructions, infrastructure objects against adverse effect of pulse and vibration loadings of a geological and technogenic origin is actual. Traditional systems of seismoprotection provide seismic stability at the expense of increase of bearing ability of designs and their connections that stimulates creation of stronger, rigid and monolithic constructions. Thus construction cost in seismic countries in comparison with not seismic increases by 4-12% depending on seismodanger size.

Use of nonconventional systems of vibroseismoprotection allows to provide safety of buildings and constructions at earthquakes and technogenic influences. Thus the budget cost of construction decreases by 3-6%, a material capacity of buildings and constructions for 5-10%, and also the scope of standard designs by control of areas with the increased seismicity extends, height of buildings increases when using the same designs.

Among nonconventional ways of vibration and seismic protection the most perspective is application of vibration and seismic isolators on the basis of rubber-metal designs. On many parameters - simplicity of production, reliability, dimensions, costs such designs surpass traditional schemes of the same appointment. They allow to find essentially new constructive solutions of responsible knots of protection of modern technical systems The analysis of world practice of vibration and seismic protection of cars, buildings and constructions shows that systems with use of rubber-metal blocks is the most perspective. Such systems allow to protect cars and buildings at seismic influences not only in the horizontal and vertical planes, but also from torsion. Besides, application of rubber-metal layered vibration isolators allows to protect buildings and the people who were in them from influences of the subway, motor and railway transport Besides, application of rubber-metal layered vibration isolators allows to protect buildings and the people who were in them from influences of the subway, auto and railway transport. The problem of calculation intense the deformed condition of polymeric elements of designs is rather actual [Lavendel E. E. 1976, Dymnikov S. I. 1968, Kirichevskiy V. V. 2005, Biderman V. L, Sukhova N. A. Malkov V. M 1998, Ray M. 2010, Dyrda V. I. 2010, Grigolyuk E. I., Kulikov G. M. 1988, Peng R. W. Landel R. F. 1975, Mooney M.A., 1940].

RESEARCH OBJECT

Rubber elements of vibration isolators have rather simple form. However conditions of loading are defined not only external loadings, but also a form of the metal elements of vibration isolators interfaced to them. Besides, rubber possesses weak compressibility. Calculation of parameters intense the deformed condition of such elements of designs probably various methods – experimental, empirical, approximate analytical, numerical. One of the main characteristics of a vibration and seismic isolators is rigidity on compression at vertical loading.

RESULTS OF RESEARCH

Let's consider the multilayered vibration isolators consisting of three metal plates of rather big thickness and two rubber blocks of a cylindrical form. For such vibration and seismic isolators during static tests rigidity on compression was defined at the various size of loading of rubber blocks: diameter 400mm, height 120mm. As a result of simple recalculations it is possible to define dependence between an deformation of a support and the enclosed loading:

$$\Delta = \frac{P}{C_{st}},\tag{1}$$

where: Δ – seismic support contraction; P – compression loading; C_{st} – vertical rigidity of a seismic support.

On the other hand, for small deformations $(\epsilon < 0.1)$ Dyrda V.I. received analytical dependence between an contraction of a cylindrical rubber layer with free end faces and enclosed loading by the method of Ritz:

$$\Delta = \frac{P_0 h}{3\pi R^2 G} \left(1 - \frac{R}{h\sqrt{6}} th \frac{h\sqrt{6}}{R} \right) \quad , \tag{2}$$

where: P_0 – compression loading on rubber layer with free end faces; h – height of a rubber layer R – radius of a rubber layer; G – module of shift of rubber.

At axial compression for small deformations (ϵ <0.1) dependence between an contraction of a rubber layer and enclosed loading is defined by a formula;

$$\Delta = \frac{P_0 h}{3\pi R^2 G} \,. \tag{3}$$

At calculation of seismic support it is necessary to consider that end faces of a rubber layer is vulcanized to metal plates. Then instead of loading P_0 it is necessary to insert the corrected value of real loading P which considers increase in rigidity at the expense of fixing of end faces into formulas (2) and (3):

$$P_0 = \frac{P}{\beta} \,, \tag{4}$$

where: $\beta = 1 + 0.413\rho^2$ [Payne A. R., 1959] or $\beta = 0.92 + 0.5\rho^2$ [Lavendel E. E., 1976].

V. I. Dyrda suggested to calculate coefficient β on a formula:

$$\beta = 1 + 0.83 \rho^2 \,, \tag{5}$$

where: $\rho = \frac{R}{h}$; β – coefficient of increase in

rigidity at the expense of fixing of end faces.

Universal numerical method of calculation of rubber vibration and seismic isolators which allows to consider asymmetry of loadings and fixing, and also to receive a full picture intense the deformed condition is finite element method. Thus the traditional final element method doesn't allow take account for a weak compressibility of rubber. For constructions from elastomers the moment scheme of finite elements with use of threefold approximation a component of a vector of movement, a tensor of deformations and function of change of volume of rubber is used. Approximating functions are accepted in the form of square polynoms:

$$\begin{split} u_i &= \omega_i^{(000)} + \omega_i^{(100)} \psi^{(100)} + \omega_i^{(010)} \psi^{(010)} + \\ &+ \omega_i^{(001)} \psi^{(001)} + \omega_i^{(110)} \psi^{(110)} + \omega_i^{(101)} \psi^{(101)} + \\ &+ \omega_i^{(011)} \psi^{(011)} + \omega_i^{(111)} \psi^{(111)} + \omega_i^{(200)} \psi^{(200)} + \\ &+ \omega_i^{(020)} \psi^{(020)} + \omega_i^{(002)} \psi^{(002)} + \omega_i^{(210)} \psi^{(210)} + \\ &+ \omega_i^{(201)} \psi^{(201)} + \omega_i^{(120)} \psi^{(120)} + \omega_i^{(211)} \psi^{(021)} + \\ &+ \omega_i^{(102)} \psi^{(102)} + \omega_i^{(120)} \psi^{(012)} + \omega_i^{(211)} \psi^{(211)} + \\ &+ \omega_i^{(121)} \psi^{(121)} + \omega_i^{(112)} \psi^{(112)}, \\ \varepsilon_{11} &= e_{11}^{(000)} + e_{11}^{(001)} \psi^{(001)} + e_{11}^{(100)} \psi^{(100)} + \\ &+ e_{11}^{(011)} \psi^{(101)} + e_{11}^{(100)} \psi^{(100)} + e_{11}^{(110)} \psi^{(110)} + \\ &+ e_{11}^{(101)} \psi^{(101)} + e_{11}^{(020)} \psi^{(020)} + e_{11}^{(102)} \psi^{(102)} + \\ &+ e_{11}^{(111)} \psi^{(111)} + e_{11}^{(001)} \psi^{(021)} + e_{11}^{(012)} \psi^{(012)}, \\ \varepsilon_{22} &= e_{22}^{(000)} + e_{22}^{(001)} \psi^{(001)} + e_{22}^{(100)} \psi^{(010)} + \\ &+ e_{22}^{(101)} \psi^{(101)} + e_{22}^{(001)} \psi^{(001)} + e_{22}^{(110)} \psi^{(110)} + \\ &+ e_{22}^{(011)} \psi^{(011)} + e_{22}^{(002)} \psi^{(002)} + e_{22}^{(102)} \psi^{(102)} + \\ &+ e_{21}^{(011)} \psi^{(111)} + e_{22}^{(001)} \psi^{(201)} + e_{22}^{(102)} \psi^{(102)}, \end{split}$$

98 YURIY KOZUB

$$\begin{split} \varepsilon_{33} &= e_{33}^{(000)} + e_{33}^{(100)} \psi^{(100)} + e_{33}^{(010)} \psi^{(010)} + \\ &+ e_{33}^{(110)} \psi^{(110)} + e_{33}^{(001)} \psi^{(001)} + e_{33}^{(200)} \psi^{(200)} + \\ &+ e_{33}^{(020)} \psi^{(020)} + e_{33}^{(101)} \psi^{(101)} + e_{33}^{(011)} \psi^{(011)} + \\ &+ e_{33}^{(210)} \psi^{(210)} + e_{33}^{(120)} \psi^{(120)} + e_{33}^{(111)} \psi^{(111)}, \\ \varepsilon_{12} &= e_{12}^{(000)} + e_{12}^{(001)} \psi^{(001)} + e_{12}^{(100)} \psi^{(100)} + \\ &+ e_{12}^{(110)} \psi^{(110)} + e_{12}^{(100)} \psi^{(100)} + e_{12}^{(101)} \psi^{(101)} + \\ &+ e_{12}^{(011)} \psi^{(011)} + e_{12}^{(002)} \psi^{(002)}, \\ \varepsilon_{13} &= e_{13}^{(000)} + e_{13}^{(100)} \psi^{(100)} + e_{13}^{(010)} \psi^{(010)} + \\ &+ e_{13}^{(001)} \psi^{(001)} + e_{13}^{(110)} \psi^{(110)} + e_{13}^{(020)} \psi^{(020)} + \\ &+ e_{13}^{(001)} \psi^{(011)} + e_{11}^{(020)} \psi^{(020)}, \\ \varepsilon_{23} &= e_{23}^{(000)} + e_{23}^{(100)} \psi^{(100)} + e_{23}^{(010)} \psi^{(010)} + \\ &+ e_{11}^{(001)} \psi^{(001)} + e_{23}^{(001)} \psi^{(001)} + e_{11}^{(200)} \psi^{(200)} + \\ &+ e_{11}^{(110)} \psi^{(110)} + e_{11}^{(101)} \psi^{(101)}, \\ \theta &= \xi^{(000)} + \xi^{(100)} \psi^{(100)} + \xi^{(101)} \psi^{(010)} + \\ &+ \xi^{(001)} \psi^{(001)} + \xi^{(101)} \psi^{(101)} + \xi^{(110)} \psi^{(110)} + \\ &+ \xi^{(001)} \psi^{(001)} + \xi^{(101)} \psi^{(101)} + \xi^{(110)} \psi^{(110)} + \\ &+ \xi^{(001)} \psi^{(001)} + \xi^{(101)} \psi^{(101)} + \xi^{(110)} \psi^{(110)} + \\ &+ \xi^{(001)} \psi^{(001)} + \xi^{(101)} \psi^{(101)} + \xi^{(110)} \psi^{(110)} + \\ &+ \xi^{(001)} \psi^{(001)} + \xi^{(101)} \psi^{(101)} + \xi^{(110)} \psi^{(110)} + \\ &+ \xi^{(001)} \psi^{(001)} + \xi^{(101)} \psi^{(101)} + \xi^{(110)} \psi^{(110)} + \\ &+ \xi^{(001)} \psi^{(001)} + \xi^{(101)} \psi^{(101)} + \xi^{(110)} \psi^{(110)} + \\ &+ \xi^{(001)} \psi^{(011)} + \xi^{(111)} \psi^{(111)}, \end{split}$$

where: u_i - components of a vector of movements; ε_{ij} - components of a tensor of deformations; θ - function of change of volume; $\omega_i^{(pqr)}$ - decomposition components; $\psi^{(pqr)}$ - a set of sedate coordinate functions of a look

$$\psi^{(pqr)} = \frac{\left(x^{1}\right)^{p}}{p!} \cdot \frac{\left(x^{2}\right)^{q}}{q!} \cdot \frac{\left(x^{3}\right)^{r}}{r!}, (p, q, r = 0, 1, 2). (7)$$

Let's find to a contraction for a two-layer seismic support under the influence of loading $P = 50\kappa N$, (the module of shift of rubber G = 0.63MPa). Dyrda V. I. Lisitsa N.I., etc. received the solution of a nonlinear task a precipitation of the continuous cylinder taking into account toughening at end faces by means of the accuracy Runge-Kutt method of the fourth order. he received value a seismic insulator precipitation ($\Delta = 0.0127m$) rather well coincides with experimental data.

The analysis of behavior of vibration and seismic isolator at imposition of cyclic or impulsive loading requires the account of viscoelastic properties of rubber elements. A viscoelasticity determines it dumping properties. For description of viscoelasticity deformation it is possible to take advantage of Volterra's equalizations

$$\sigma = E_0 \left[\varepsilon - \int_0^t R(t - \tau) \varepsilon(\tau) d\tau \right]. \tag{8}$$

where: $R(t-\tau)$ – kernel of relaxation.

In addition, for description of behavior of nearly incompressible material different nonlinear laws are used. For example, Peng-Landel's law [Peng R. W., Landel R. F., 1975.]

$$\sigma^{ij} = I_3^{1/2} \left[\mu \left(\left(-I_3^{-1/3} + \frac{2}{9} (2I_1 - 3)(I_3 - 1) \right) G^{ij} + H_3^{-4/3} g^{ij} \right) + \frac{B}{2} (I_3 - 1) G^{ij} \right],$$
(9)

where: I_1 , I_3 are invariants of tensor of deformations; μ , B are constant of material, G^{ij} is a metrical tensor.

We replace resilient permanent is the module of compression $\it B$ and module of shear $\it \mu$ we get the Volterra's operators

$$\sigma^{ij} = I_3^{1/2} \left[\mu \left(\left(-I_3^{-1/3} + \frac{2}{9} (2I_1 - 3)(I_3 - 1) \right) G^{ij} + \right. \\ \left. + I_3^{-4/3} g^{ij} \right) + \frac{B}{2} (I_3 - 1) G^{ij} - \right. \\ \left. - \mu \int_{-\infty}^{t} R_{\mu} (t - \tau) \left(-I_3^{-1/3} + \frac{2}{9} (2I_1 - 3)(I_3 - 1) \right) G^{ij} d\tau - \right. \\ \left. - \mu \int_{-\infty}^{t} R_{\mu} (t - \tau) I_3^{-4/3} g^{ij} G^{ij} d\tau \right. \\ \left. - \frac{B}{2} \int_{-\infty}^{t} R_b (t - \tau) (I_3 - 1) G^{ij} d\tau \right].$$
(10)

The tensor of deformations can be presented as a sum linear and nonlinear constituents

$$\varepsilon_{ij} = \varepsilon_{ij}^{l} + \varepsilon_{ij}^{n},$$

$$\varepsilon_{ij}^{l} = \frac{1}{2} \left(c_{j}^{k} u_{k,i} + c_{i}^{k} u_{k,j} \right),$$

$$\varepsilon_{ij}^{n} = \frac{1}{2} u_{k,i} u_{i,j}^{k}.$$
(11)

Then the invariants of Cauchy- Green's tensor of deformations also can be presented as a sum linear and nonlinear parts

$$I_{1} = I_{1}^{l} + I_{1}^{n},$$

$$I_{1}^{l} = \varepsilon_{11}^{l} + \varepsilon_{22}^{l} + \varepsilon_{33}^{l},$$

$$I_{1}^{n} = \varepsilon_{11}^{n} + \varepsilon_{22}^{n} + \varepsilon_{33}^{n}.$$
(12)

We put (12) in (10) and we lay out I_3 in the Taylor series about with $I_3 = 1$ as the center of the circle of convergence. Then we cast aside by virtue of weak compressibility of material members of decomposition the second order of trifle and we get the linearized correlation. For the decision of task of nonlinear deformation of constructions different methods are used [Dymnikov S.I., 1968, Lavendel E.E., 1980, Kirichevskiy V.V., 2005]. Most effective among them is the modified Newton-

Kantorovich method. At the use of this going near the decision of task on every step on loading get the specified linearized equalization

$$Ku^{i+1} = -N(u^i) - P_k$$
, (13)

where: K is matrix of inflexibility of construction; $N(u^i)$ is a vector of the nonlinear additions, conditioned by physical and geometrical non-linearity; P_k is vector of key forces; u is a vector of the key moving. On the basis of this approach the task of determination is decided seismic support.

The problem is also solved on the basis of the moment scheme of finite elements on the basis of the obtaining complex «MIRELA+». In fig. 1-4 are presented finite element model and distribution of movements and tension in the radial section of a rubber element

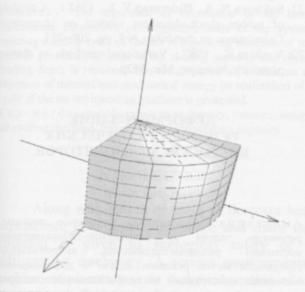


Fig. 1. Finite element model

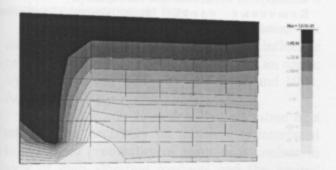


Fig. 2. Axial movement

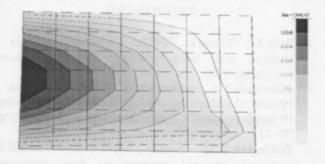


Fig. 3. Radial movement

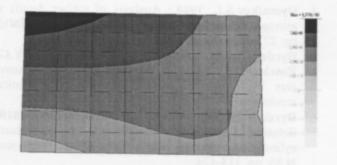


Fig. 4. Stress σ_{12}

As comparison we will give a calculation example a precipitation of a rubber layer of a seismic support on formulas (2) and (3). Results of calculations are given in table.

Table. Seismic support contraction

Indicator	Experiment	For	mula	FEM
		(2)	(3)	1.1600 100
Δ, m	0.012	0.0084	0.0128	0.0122

CONCLUSIONS

The method of calculation of vibration and seismic isolators is developed. The analysis of the received results shows that use of a finite element method allows to receive a complete picture of distribution of tension and movements on the volume of an element of a design taking into account weak compressibility of a material.

REFERENCES

- Bate K., Vilson E., 1982.: Numerical methods of analisys and finite element method. Moscow, Stroyizdat, 470p.
- Biderman V.L. Sukhova N.A., 1968.: Calculation of cylindrical and rectangular long rubber shock-absorbers of compression. Calculations on durability. N 13. pp. 55–72.
- Dokhnyak B.M., Kozub Y.G., 2002.: Account of previously stressed constructions from elastomers. Proc. 13 Symp. "Problems of tyres and rubber-cord composits", 14–18 October, Moscow, SRITI, pp. 119–123.
- Dymnikov S.I., 1968.: Analysis of rubber details at average deformations. Mechanics of polymers. N 2. pp. 271-275.
- Dyrda V.I., Agaltsov G.N., Kozub Y.G., Roschupkin S.V., 2010: Vibration protection of heavy cars by means of rubber elements. Geotechnical mechanics. N 86. pp. 171-195.
- Dyrda V.I., Goncharenko A.V., Zharko L.V., 2010.: Solution of a task on compression of the viscoelastic cylinder by a method Ritz's. Geotechnical mechanics. N 86. pp. 113-124.
- Dyrda V.I., Maryenko N.G., 2009.: Analysis and choice of parameters of rubber-metal seismic support. Geotechnical mechanics. N 84. – pp. 17–23.
- Grigolyuk E.I., Kulikov G.M., 1988.: Multilayered reinforced covers. Moscow, Mashinostroyenie, 288p.
- Kirichevskiy V.V. Dokhnyak B.M. Kozub Y.G., Gomenyuk S.I., Kirichevskiy R.V., Grebenyuk S.N., 2005.: Finite element method in obtained complex "MIRELA +". Kyiv, Nukova dumka, 403p.
- Kirichevskiy V.V., 2002.: Finite element method in mechanics of elastomers. Kyiv, Naukova dumka, 655p.
- 11. Kirichevskiy V.V. Dokhnyak B.M., Vysotskaya N.D., Kozub Y.G., 1992.: FEM in the nonlinear viscous elasticity of elastomer constructions. Proceeding of 6 International Scientific and Technical Conf. "ELASTOMERS", Riga, p.97.
- Lavendel E.E., 1976.: Calculation of rubber products: monograph. Moscow, Mashinostroyenie, 232p.
- Lavendel E.E., 1980.: Methods of applied calculation for production from high elasticity materials. Riga, Zinatne, 238c.

- Malkov V.M., 1998.: Mechanics of multilayed elastomeric constructions. Sant-Petersburg, 320p.
- Mooney M.A., 1940.: Theory of Large Elastic Deformation. J. Appl. Phys, N 11, pp. 582–592.
- Ogden R. W., 1972.: Large deformation isotropic elasticity on correlation of theory and experiment for incompressible rubber-like solids. Proc. Roy. Soc. London. Ser. A, Vol. 326, pp.565-584.
- Payne A. R., 1959.: Shape factors and functions in rubber engineering. Engineer, Vol. 207, N 5379, pp. 51–59.
- 18. Peng R. W., Landel R. F., 1975.: Stored energy function and compressibility of compressible rubber like materials under large straine. J. Appl. Phys, N 6, Vol.46, pp. 2599–2604.
- 19. Ray A., Ray M., 2010.: Anvil-block vibration damping by means of friction force. TEKA Commission of Motorization and Power Industry in Agriculture, OL PAN, 10C, Lublin, pp. 242–249.
- 20. Ray R., Ray M., 2010.: The definition of reactions of motion system of no-anvil hammer. TEKA Commission of Motorization and Power Industry in Agriculture, OL PAN, 10C, Lublin, pp. 250-254.
- Sukhova N. A., Biderman V. L., 1962.: Calculation of rubber shock-absorbers worked on compression. Calculations on durability, N 8, pp. 200–211.
- Vashizu K., 1987.: Variational methods in elasticity plasticity. Moscow, Mir, 542p.

ДЕФОРМИРОВАНИЕ РЕЗИНОМЕТАЛЛИЧЕСКИХ ВИБРОСЕЙСМОИЗОЛЯТОРОВ

Юрий Козуб

Аннотация. Рассмотрены различные подходы к решению задачи о напряженно-деформированном состоянии резинометаллических виброизоляторов. Предложен метод решения задачи о деформировании элементов конструкций из слабосжимаемого материала основанный на применении моментной схемы конечных элементов. Для решения задачи нелинейного вязкоупругого деформирования конструкции используется метод Ньютона-Канторовича.

Ключевые слова. Метод конечных элементов, виброизолятор, слабая сжимаемость.